PROBLEMS

1) An ice cream mix formulation having a viscosity of 70 centipoises and a density of 1050 kg/m³ is being canned aseptically at the rate of 20 L/min. The mix is heated to 285°F, passed through a 100 ft long 0.870 in inside diameter stainless steel pipe and cooled. Calculate the sterilizing value of this process ($D_0 = 1.83$ min, Z = 24°F, 1000 L = 1 m³, 1 in = 2.54 cm)

Solution:

$$Q = 20 \frac{L}{min} \times \frac{1 dm^3}{1L} \times \frac{1m^3}{(10 dm)^3} = 0.02 \frac{m^3}{min}$$

Djameter = 0.087 in = 0.0221 m

$$r = \frac{0.0221}{2} = 0.04105 m$$

Vaug = $\frac{Q}{A} = \frac{0.02 \frac{m^3}{min}}{11 \times (0.01105 m)^2} = 52.138 \frac{m}{min}$
Vaug = $52.138 \frac{m}{min} \times \frac{1min}{605} = 0.868 \frac{m}{5}$
 $Re = \frac{P. Vaug \cdot D}{M} = \frac{(1015)(0.868)(0.0221)}{70 \times 10^{-3}}$
 $(70 cp = 0.07 poise = 0.07 Pa.5)$
 $Re = 278.15 < 2100 = 0.07 Pa.5$
 $Re = 2.138 = 104.276 \frac{m}{min}$

$$F = \frac{L}{V_{max}} = \frac{100 ft \times \frac{12 in}{16t} \times \frac{2.5 hom}{1in} \times \frac{1m}{1ppom}}{104.776 \text{ m/min}} \Rightarrow$$

$$F_{285} = 0.292 \text{ min}$$

$$Log \frac{D_{285}}{D_0} = \frac{T_0 - T_{285}}{2} = \frac{250 - 285}{2h} = -1.458$$

$$\frac{D}{285} = 10^{-1.458} \Rightarrow D_{285} = D_{0} \times 0.0348$$

$$D_{285} = 1.83 \times 0.0348 = 0.0636 \text{ min}.$$

$$SV = \log \frac{N_0}{N} \quad j \quad F_{285} = D_{285} \times (SV)_{285}$$

$$SV_{285} = \frac{F_{285}}{D_{285}} = \frac{0.292 \text{ min}}{0.0636 \text{ min}} = \frac{4.58}{2}$$

2) Homework: A thermocouple located at the slowest heating point (the center of can) of a picnic can insulated by other cans at the both ends indicated the following temperature-time relationships (the retort temperature is 240°F):

Time (min)	0	10	30	40	50	60	75
T (°F)	140	160	212.5	225	230.5	235	110

Determine the process time by graphical method. The F_0 value for *Cl. botulinum* upon which the process is to be based is 2.55 min and $Z = 18^{\circ}F$ for 250°F. Determine whether this process would be a safe process. If it is not, what would you recommend ?

3) The Do value of *Cl. botulinum* in a product is 0.3 min. At the pH of the product, the Do value of PA 3679 botulinum is 1.5 min. When conducting an inoculated pack, how many spores of PA 3679 botulinum must be introduced per can such that a spoilage rate of 1/100 cans would satisfy a 20D reduction of PA 3679 *Cl. botulinum* ?

Solution:

$$F_{0} = D_{0} \cdot (SV) = 0,3 \times 20 = 6 \min$$

$$\frac{1}{20D} \text{ reduction}$$

$$N_{f} = \frac{1}{100} = 0,01$$

$$\log \frac{N_{0}}{N_{f}} = \frac{F_{0}}{D_{0}} = 3\log \frac{N_{0}}{0,01} = \frac{6}{1.5} = 3N_{0} = 100 \text{ spones}$$

$$\log \frac{N_{0}}{N_{f}} = \frac{F_{0}}{D_{0}} = 3\log \frac{N_{0}}{0,01} = \frac{6}{1.5} \text{ must be introduced}.$$

4) Cans of a given food were heated in a retort for sterilization. The Fo for *Cl. botulinum* in this type of food is 2.50 min and Z value is 18°F. The temperatures in the center of a can were measured and were approximately as follows (the average temperature during each time period was listed below:

t₁ :(0-20 min), T₁:160 °F; t₂:(20-40 min), T₂:210 °F; t₃:(40-57 min), T₃:235 °F

Determine if this sterilization process is adequate using mathematical model.

Solution:

$$F_{o} = \sum t \times 10^{-\frac{1}{2}}$$

$$F_{o} = 20 \times 10^{-\frac{160-250}{18}} + 20 \times 10^{-\frac{210-250}{18}} + 17 \times 10^{-\frac{235-250}{18}} =)$$

$$F_{o} = 2.615$$
Since F process (2.615) > F_{o} given (2.50) =)
the sterilization process is adequate.

5) Homework: (how to use D and Z values in pasteurization calculations):

Pooled raw milk at the processing plant has bacterial population of 4x10⁵/mL. It is to be processed at 79°C for 21 seconds. The average D value at 65°C for the mixed population is 7 min. The Z value is 7°C. How many organisms will be left after pasteurization? What time would be required at 65°C to accomplish the same degree of lethality?

6) In a given pasteurization process the reduction in the number of viable cells used is 10¹⁵ and the Fo value used is 9 min. If the reduction is increased by 10¹⁶ times because of increased contamination, what would be the new Fo value ?

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Solution:

$$\left(\frac{N_{\sigma}}{N_{f}} \right)_{1}^{2} = 10^{15}, \quad (SV)_{1}^{2} = \log \frac{N_{\sigma}}{N_{f}} = \log (10^{15}) = 15$$

$$F_{\sigma} = (SV) \cdot D_{\sigma} => 9 = 15 \times D_{\sigma} => D_{\sigma} = 0.6 \text{ min}$$

$$\left(\frac{N_{\sigma}}{N_{f}} \right)_{2}^{2} = 10^{16}, \quad (SU)_{2}^{2} = \log (10^{16}) => (SJ)_{2}^{2} = 16$$

$$\left[F_{\sigma} = (SV) \times D_{\sigma} \right]_{2}^{2} = 16 \times 0, 6 \text{ min} = 9.6 \text{ min}.$$

7) Apple juice (contains vegetative m.o.) has a viscosity of 5 cp (centi poise) and a density of 1019 kg/m³. It is to be pasteurized in a continuous system that involves to 95°C holding in a 4 in nominal pipe and cooling. When the sealed tubes (1 mL each) containing equal number of spores of vegetative organisms were heated for 1 and 1.5 min at 95°C, the survivors were 1000 and 100, respectively. (The inside radius of a 4 in pipe is 40 mm).

a) Calculate the length of holding tube for both cases when the flow rate of apple juice is 80 L/min.

b) What would be the length of holding tube for this type of foods containing vegetative microroganisms (assume SV = 5 for vegetative m.o.).

Solution:

9) First, calculate Do value at 95°C =>
f t₁ = 1 min, Nf = 1000
F t₂ = 1.5 min, Nf = 100
F = D × log
$$\frac{No}{Nf}$$
 or F = D × (SV)
1) 1 min = D × log $\frac{No}{1000}$ => D = $(\frac{1}{log No - log 100})$
2) 1.5 min = D × log $\frac{No}{1000}$ [log No - log 100]
1.5 = $\frac{1}{log No - 2}$ [log No - log 100]
1.5 = $\frac{log No - 2}{log No - 3}$ => log No = 5 => No = 1000000
Substitute into eqn (1) or (2) =>
1 = D × log $\frac{100000}{1000}$ => D = 0.5 min at 95°C
Vaug = $\frac{Q}{A} = \frac{0.08 \text{ m}^3/\text{min}}{1 \times (0.04)^2 \text{m}^2}$ = 15.91 m = 0.265 m/s

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$$Re = \frac{D.Vaug \times f}{M} = \frac{0.08 \times 0.265 \times 1019}{5 \times 10^{-3}} = 4324 > 2100 = 1$$

Flow is turbulent.
$$Vmax = \frac{Vaug}{0.0336 \times \log ke + 0.662} = 1$$

$$V_{max} = \frac{0,265}{0,0336 \times \log(4324) + 0,662} = 0,337 \text{ m/s}$$

$$F_{1} = \frac{L_{1}}{V_{max}} = L_{1} = 0,337 \text{ m} \times 1.5 \text{ m/m} \times \frac{605}{1 \text{ mm}} = 1$$

$$L_{1} = 30,33 \text{ m} (\text{Length of holding tube for} \\ 1.5 \text{ min heating})$$

$$F_2 = \frac{L_2}{Vmax} \Rightarrow L_2 = 0.337 \times 1 \times 60 = 20.22 m$$
(For heating 1 min)
(For heating 1 min)
b) For vegetative m.o., spoilage should be one can in 1 \times 10^5 cans, i.e., $SV = 5$.

$$\log \frac{N_o}{N_f} = 5$$
, $F = D \times (SV) = 0.5 \times S = 2.5 \text{ min.}$
 ${}^{5}F_{gS} = D_{gS}^{*}(SV)$

8) The following temperature history resulted from the slowest heating point of a heat penetration run on a certain low acid canned food product:

point of a heat penetration run on a certain low acid canned food product:

$$(T_- 250)/8$$

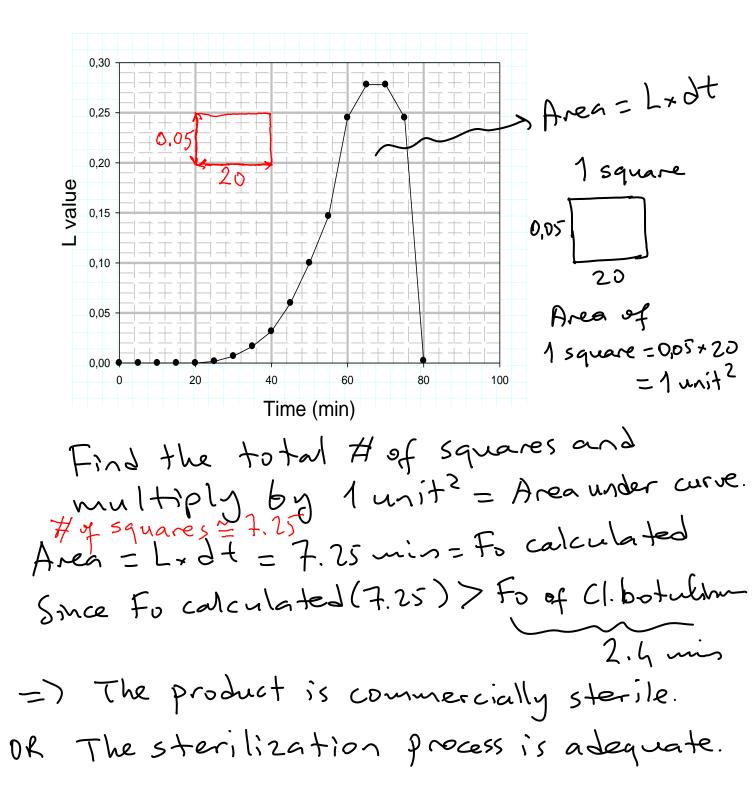
Calculate L values \longrightarrow L=10

<u>Time (min)</u>	<u>T (°F)</u>	$\underline{\mathbf{L}} = 10^{(\mathrm{T-To})/\mathrm{z}} \qquad -\mathbf{F}$
0	141	0,000 ~>> 8.8×10 -4
5	149	$\frac{1-10}{0,000} \longrightarrow 8.8 \times 10^{-7}$ $0,000 \longrightarrow 2.45 \times 10^{-6}$
10	162	
15	172	0,000 ~ 4.64 × 10
2	189	0,000 ~ 4.1× 10-7
25	200	$0,000 \rightarrow 1.5 \times 10$ $0,000 \rightarrow 4.64 \times 10^{-5}$ $0,000 \rightarrow 4.1 \times 10^{-5}$ $0,002 \rightarrow 1.66 \times 10^{-7}$
30	211	0,007
35	218	0,017
40	223	0,032
45	228	0,060
50	232	0,100
55	235	0,147
60	239	0,245
65	240	0,278
70	240	0,278

75	239	0,245	
80	202	0.002	

Does this process impart commercial sterility with respect to *Cl. botulinum* (i.e., if the sterilization process is adequate or not) using graphical method ? The Fo value for *Cl. botulinum* is 2.40 min, $Z = 18^{\circ}F$, To = 250°F.

Solution:



9) A process is based on an Fo value of 2.88 min. If a can contained 10 spores of organisms having a Do value of 1.5 min, then, calculate the probability of spoilage from the later organism.

Solution:

$$F_{0} = D_{0} \times SV, \quad SV = \log \frac{N_{0}}{N_{f}} = \frac{F_{0}}{D_{0}} = \frac{7.88}{1.5} = 1.92$$

$$\log \frac{N_{0}}{N_{f}} = 1.92 = 0 \log N_{0} - \log N_{f} = 1.92$$

$$\log N_{f} = \log N_{0} - 1.92 = \log 10 - 1.92 = -0.92$$

$$\log N_{f} = -0.92 = 0.12 = 0.12 = 0.12$$

$$\Pr = 0.12 = 0.12 = 0.12$$

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10) The Fo for *Cl. botulinum* type B is 1.1 min for 99.999 % inactivation. If the $Z = 18^{\circ}F$, what would F be at 275°F ? Also, calculate F at 275°F for 99.9999 % inactivation.

Solution:

Assume 100 spores initially =>

$$F_0 = 1.1 \text{ min}, SV = \log \frac{N_0}{N_F} = \log \frac{100}{(100 - 99.999)} =>$$

 $SV = 5$
 $\log \frac{f_275}{F_0} = \frac{T_0 - 275}{18} => \log \frac{f_275}{1.1} = \frac{250 - 275}{18} =>$

$$F_{275} = 0.0449 \text{ min.}$$

$$F_{275} = D_{275} \times SV_{275} = 0.0449 = D_{275} \times \log \frac{100}{100 - 99.999}$$

$$D_{275} = \frac{0.0449}{5} = 0.00898 \text{ min}$$

$$F_{07} \quad 99.9999 \% \text{ mactivation at } 275^{\circ}F = 3$$

$$F_{275} = D_{275} \times SV_{275} = 3$$

$$F_{275} = 0.00898 \times \log \frac{100}{100 - 99.9999}$$

$$F_{275} = 0.00898 \times 6 = 0.054 \text{ min heating}$$
is required at $275^{\circ}F$ for 99.9999 % inactivation of microorganism.

11) Browning reaction in the milk has been shown to have a Q_{10} of 1.585. If this product is processed at 285°F and 260°F to an Fo = 15 min in the holding tube of an aseptic canning system, compare the extent of formation of the brown pigment between the product processed at these temperatures, i.e., $C_{260}/C_{285} = ? Z = 22$ °F. Assume a zero order kinetics for formation of brown pigment and initial concentration of pigment is zero. Solution:

$$F_0^{22} = 15 \text{ min}, \quad f_{260}^{=?}, \quad F_{285}^{=?}, \quad F_{$$

$$\frac{F}{F_{o}} = 10^{\frac{250-T}{2}}$$

$$\frac{F}{F_0} = \frac{F_{260}}{F_0} = 10^{\frac{250-260}{22}} = 3\frac{F_{260}}{15} = 10^{-0.454} = 0.351$$

= $F_{260} = 15 \times 0,351 = 5,266$ -351.

$$\frac{F_{285}}{F_0} = \frac{F_{285}}{15} = 10^{-285} \implies F_{285} = 0,384 \text{ min}$$

$$\frac{k_{285}}{k_{260}} = 1.585$$

$$k_{285} = (1.585 \times k_{260})$$

$$C_{260} = k_{260} \times F_{260})$$

$$C_{285} = k_{285} \times F_{285}$$

$$\frac{C_{260} = k_{260} \times 5.266}{C_{285}} , C_{285} = 1.585 \times k_{260} \times 0.384$$

$$\frac{C_{285} = 1.585 \times k_{260} \times 0.384}{0.608} = 8.66 \Rightarrow \frac{C_{260}}{C_{285}} = 8.66$$

$$\therefore \text{ There would be } 8.66 \text{ times more}$$
intense browning in the 260°F processed
product compared to the one processed
at 285°F.