

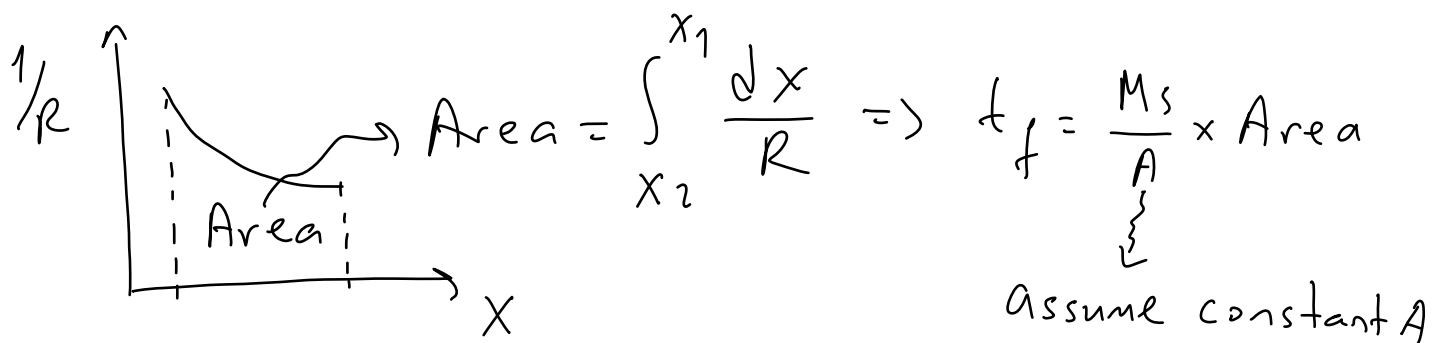
Calculation Methods for Falling Rate Drying Period:

⊗ Method using graphical integration:

$$t_f = \frac{M_s}{A} \times \int_{x_2}^{x_1} \frac{dx}{R} = \frac{M_s}{A} \int_{x_2}^{x_1} \frac{1}{R} \cdot dx$$

From drying data find several R values \Rightarrow

i.e., $\frac{R}{\vdots}$ vs $\frac{x}{\vdots}$ and calculate $\frac{1/R}{\vdots}$



We assume negligible shrinkage \Rightarrow

A = constant.

If A \neq constant \Rightarrow A = f(x) = A(x)

\Rightarrow integrate it.

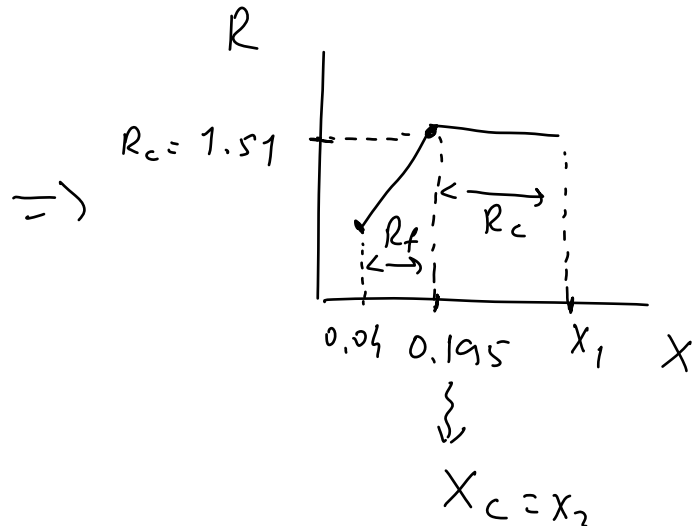
$$t_f = M_s \times \int_{x_2}^{x_1} \frac{dx}{A(x) \cdot R} \rightsquigarrow \text{if } A \neq \text{constant}$$

Example: A batch of wet solid whose data are given below is to be dried from a moisture content of $X_1 = 0.38$ to $X_f = 0.04$ kg H₂O/kg DS. The weight of the dry solids is $M_s = 399$ kg and $A = 18.58$ m² of top drying surface.

Calculate the time for drying. (Given that $R_c = 1.51$ kg H₂O/h.m²).

For falling rate period:

X	R	$1/R$
$X_c = 0.195$	1.51	✓
0.150	1.21	✓
0.100	0.90	✓
0.065	0.71	✓
0.50	0.37	✓
0.04	0.27	✓



Solution: Find $1/R$ values \Rightarrow

$$\frac{M_s}{A} = \frac{399}{18.58} = 21.5 \text{ kg/m}^2$$

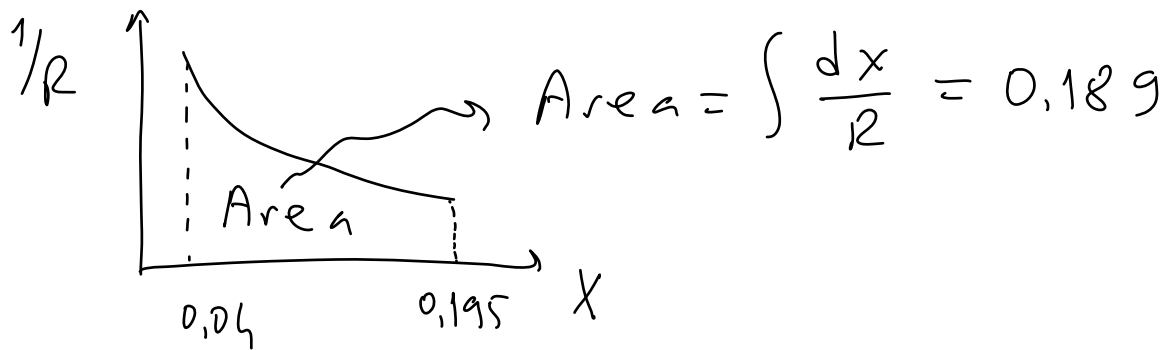
$$t_c = \frac{M_s}{A \times R_c} \times (X_1 - X_2), \quad X_1 = 0.38, \quad X_2 = X_c = 0.195$$

$$t_c = 21.5 \times \frac{1}{1.51} \times (0.38 - 0.195) = 2.63 \text{ h}$$

Σ in the falling rate period $\Rightarrow t_f = ?$

Find t_f graphically \Rightarrow

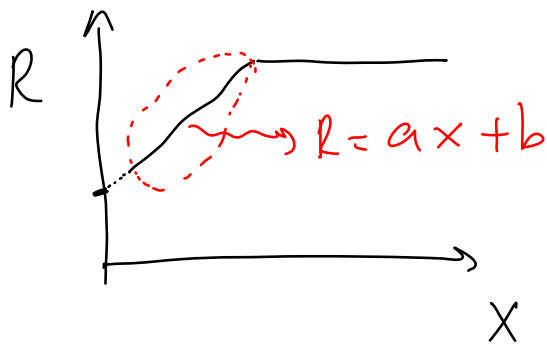
$$t_f = \frac{M_s}{A} \int_{x_2}^{x_1} \frac{dx}{R} \quad \Rightarrow$$



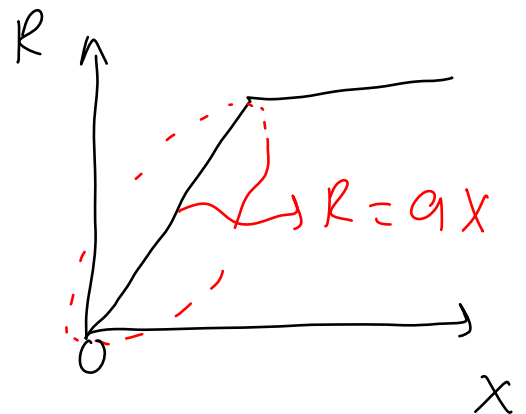
$$t_f = 21.5 \times (0.189) = 4.06 \text{ h}$$

$$\text{total drying time} = t_c + t_f = 2.63 + 4.06 = 6.69 \text{ h.}$$

⊗ Calculation methods for special cases in falling rate period:



OR



1) Rate is linear function of X .

ie., $R = ax + b \Rightarrow$ differentiate it \Rightarrow

$$t_f = \frac{M_s}{A} \int_{x_2}^{x_1} \frac{dx}{R}$$

$$dR = a \cdot dx \Rightarrow dx = \frac{dR}{a} \Rightarrow$$

$$t_f = \frac{M_s}{A} \times \int_{x_2}^{x_1} \frac{1}{a} \times \frac{dR}{R} = \frac{M_s}{a \cdot A} \int_{R_2}^{R_1} \frac{dR}{R} \Rightarrow$$

$$t_f = \frac{M_s}{a \cdot A} \times \ln \frac{R_1}{R_2}$$

Since $R_1 = a \cdot x_1 + b$

+ $R_2 = a \cdot x_2 + b$

$$R_1 - R_2 = a(x_1 - x_2) \Rightarrow a = \frac{R_1 - R_2}{x_1 - x_2}$$

$$t_f = \frac{M_s}{A} \times \frac{(x_1 - x_2)}{(R_1 - R_2)} \times \ln \frac{R_1}{R_2}$$

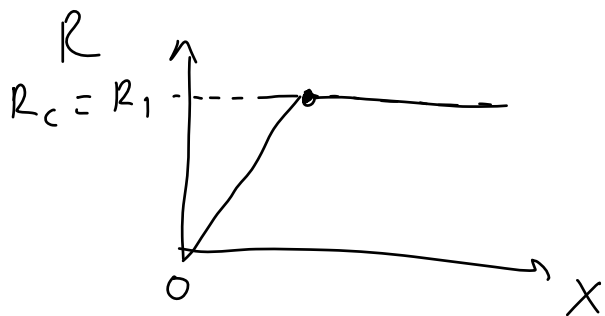
2) Rate is a linear function through origin:

$$R = aX \Rightarrow \text{differentiate} \Rightarrow dR = a \cdot dx \Rightarrow$$

$$dx = \frac{dR}{a}$$

$$t_f = \frac{M_s}{A} \int_{x_2}^{x_1} \frac{dx}{R} \Rightarrow$$

$$t_f = \frac{M_s}{A} \int_{R_2}^{R_1} \frac{1}{a} \times \frac{dR}{R} = \frac{M_s}{a \cdot A} \times \ln \frac{R_1}{R_2}$$



$$R_1 = a X_1$$

$$R_2 = a X_2$$

$$R_1 - R_2 = a (X_1 - X_2)$$

$$a = \frac{R_1 - R_2}{X_1 - X_2}$$

$$\text{If } R_1 = R_c \Rightarrow X_1 = X_c$$

$$X_2 = 0 \Rightarrow R_2 = 0 \Rightarrow a = \frac{R_1}{X_1} = \frac{R_c}{X_c}$$

$$t_f = \frac{M_s}{A \times \frac{R_c}{X_c}} \times \ln \left(\frac{R_c}{R_2} \right)$$

$$\Rightarrow \boxed{t_f = \frac{M_s}{A} \times \frac{X_c}{R_c} \times \ln \frac{X_c}{X_2}}$$

$$\frac{R_c}{R_2} = \frac{a \cdot X_c}{a \cdot X_2} = \frac{X_c}{X_2}$$

$$\boxed{R_f = R_c \times \frac{X}{X_c}}$$

Example: Repeat the previous example, but as an approximation assume a straight line of the rate R vs X through the origin from point X_c to $X = 0$ for the falling rate.

Solution: $R = a \cdot X \rightarrow$ straight line passing through origin.

$$R_c = 1.51, \quad X_c = 0.195, \quad X_2 = 0.04$$

$$t_f = \frac{M_s}{A} \cdot \frac{X_c}{R_c} \times \ln \frac{X_c}{X_2} = \left(\frac{399}{18.58} \right) \times \frac{0.195}{1.51} \times \ln \frac{0.195}{0.04}$$

$$t_f = 4.39 \text{ h.}$$

Moisture Diffusivities in Foods.

⊗ If a diffusion transport mechanism is assumed \Rightarrow

the rate of moisture movement is described by an effective diffusivity value, D_{eff} .

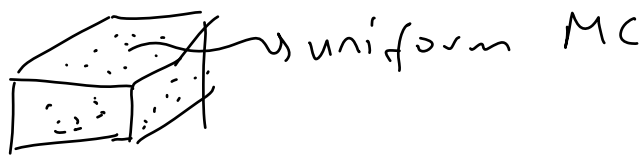
⊗ D_{eff} represents the overall transport property of water in the food. It includes the effect of liquid diffusion, vapor diffusion, etc.,

* Fick's law is often used to describe a moisture diffusion process.

$$\frac{\partial X}{\partial t} = D_{\text{eff}} \times \frac{\partial^2 X}{\partial L^2}$$

Assumptions:

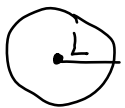
- 1) Constant diffusivity
- 2) Uniform initial MC



- 3) A zero moisture gradient at the center of the sphere.



* Solution of Fick's Law for a Sphere:



$$m^* = \frac{X - X^*}{X_0 - X^*} = \frac{6}{\pi^2} \times \sum_{n=1}^{\infty} \exp\left(-n^2 \times \frac{D_{\text{eff}} \times \pi^2}{L^2} \times t\right)$$

for long drying periods take $n=1$

$$M^* = \frac{X - X^*}{X_0 - X^*} = \frac{6}{\pi^2} \times \exp\left(-\frac{D_{eff} \cdot \pi^2 \cdot t}{L^2}\right)$$

$X = Mc$ at any time

X^* = equilibrium MC

X_0 = initial MC

t = drying time

D_{eff} = effective diffusion coefficient

D_{eff} : m^2/s or cm^2/s

L = radius of sphere

For most of the foods D_{eff} : 10^{-9} to $10^{-12} \text{ m}^2/\text{s}$.

If $D_{eff_1} = 10^{-9}$ and $D_{eff_2} = 10^{-11} \text{ m}^2/\text{s}$ =>

drying is faster.

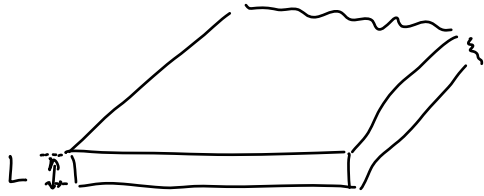
⊛ Solution of Fick's Law for a Slab:

$$M^* = \frac{X - X^*}{X_0 - X^*} = \frac{8}{\pi^2} \cdot \sum_{n=0}^{\infty} \frac{1}{(2n+1)^2} \times \exp\left[-\frac{(2n+1)^2 \cdot \pi^2 \cdot D_{eff} \cdot t}{4 \times L^2}\right]$$

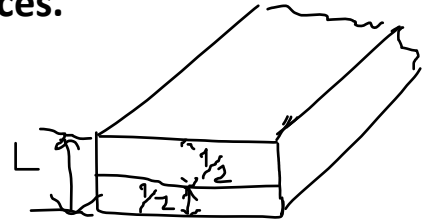
For long drying times => $n=0$ only =>

$$m^* = \frac{x - x^*}{x_0 - x^*} = \frac{8}{\pi^2} \cdot \exp\left(-\frac{\pi^2 \cdot D_{eff} \cdot t}{4 \cdot L^2}\right)$$

L : thickness of the slab.



$L = 1/2$ the thickness of the slab when drying occurs from the top and the bottom parallel faces.



⊗ Solution of Fick's Law for a Cylinder:

$$m^* = \frac{x - x^*}{x_0 - x^*} = \frac{4}{L^2} \times \sum_{n=1}^{\infty} \frac{1}{\beta_n^2} \exp(-D_{eff} \cdot \beta_n^2 \cdot t)$$

L : radius of cylinder



β_n : Bessel function

at large drying times $\Rightarrow n=1 \Rightarrow$

$$m^* = \frac{x - x^*}{x_0 - x^*} = \frac{4}{L^2} \times \frac{1}{\beta_n^2} \cdot \exp(-D_{eff} \cdot \beta_n^2 \cdot t)$$